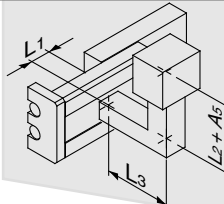


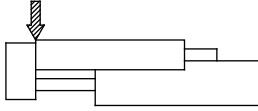
Series MXS Model Selection

Model Selection Steps	Formula/Data	Selection Examples				
1 Operating Conditions List the operating conditions considering the mounting position and workpiece configuration.	- Model to be used - Type of cushion - Workpiece mounting position - Mounting orientation - Average speed V_a (mm/s) - Load mass W (kg): Fig. (1) - Overhang L_n (mm): Fig. (2)	 Cylinder: MXS16-50 Cushion: Rubber bumper Workpiece table mounting Mounting: Horizontal wall mounting Average speed: $V_a = 300$ [mm/s] Load mass: $W = 1$ [kg] $L_1 = 10$ mm $L_2 = 30$ mm $L_3 = 30$ mm				
2 Kinetic Energy Find the kinetic energy E (J) of the load. Find the allowable kinetic energy E_a (J). Confirm that the kinetic energy of the load does not exceed the allowable kinetic energy.	$E = \frac{1}{2} \cdot W \cdot \left(\frac{V}{1000}\right)^2$ Collision speed $V = 1.4 \cdot V_a$ *) Correction factor (Reference values) $E_a = K \cdot E_{max}$ Workpiece mounting coefficient K: Fig. (3) Max. allowable kinetic energy E_{max}: Table (1) Kinetic energy (E) $\leq$ Allowable kinetic energy (E_a)	$E = \frac{1}{2} \cdot 1 \cdot \left(\frac{420}{1000}\right)^2 = 0.088$ $V = 1.4 \times 300 = 420$ $E_a = 1 \times 0.11 = 0.11$ Can be used based on $E = 0.088 \leq E_a = 0.11$				
3 Load Factor						
3-1 Load Factor of Load Mass Find the allowable load mass W_a (kg). Note) There is no need to consider this load factor in the case of using perpendicularly in a vertical position. (Define $\alpha_1 = 0$.) Find the load factor of the load mass α_1.	$W_a = K \cdot \beta \cdot W_{max}$ Workpiece mounting coefficient K: Fig. (3) Allowable load mass coefficient β: Graph (1) Max. allowable load mass W_{max}: Table (2) $\alpha_1 = W/W_a$	$W_a = 1 \times 1 \times 4 = 4$ $K = 1$ $\beta = 1$ $W_{max} = 4$ $\alpha_1 = 1/4 = 0.25$				
3-2 Load Factor of Static Moment Find the static moment M (N·m). Find the allowable static moment M_a (N·m). Find the load factor α_2 of the static moment.	$M = W \times 9.8 \times (L_n + A_n)/1000$ Correction value of moment center position distance A_n: Table (3) $M_a = K \cdot \gamma \cdot M_{max}$ Workpiece mounting coefficient K: Fig. (3) Allowable moment coefficient γ: Graph (2) Maximum allowable moment M_{max}: Table (4) $\alpha_2 = M/M_a$	<table><tr><th>Yawing</th><th>Rolling</th></tr><tr><td>Examine M_y. $M_y = 1 \times 9.8 \times (10 + 30)/1000 = 0.39$ $A_3 = 30$ $M_{ay} = 1 \times 1 \times 15.9 = 15.9$ $M_{ymax} = 15.9$ $K = 1$ $\gamma = 1$ $\alpha_2 = 0.39/15.9 = 0.025$</td><td>Examine M_r. $M_r = 1 \times 9.8 \times (30 + 10)/1000 = 0.39$ $A_6 = 10$ $M_{ar} = 15.9$ (Same value as M_{ay}) $\alpha_2 = 0.39/15.9 = 0.025$</td></tr></table>	Yawing	Rolling	Examine M_y . $M_y = 1 \times 9.8 \times (10 + 30)/1000 = 0.39$ $A_3 = 30$ $M_{ay} = 1 \times 1 \times 15.9 = 15.9$ $M_{ymax} = 15.9$ $K = 1$ $\gamma = 1$ $\alpha_2 = 0.39/15.9 = 0.025$	Examine M_r . $M_r = 1 \times 9.8 \times (30 + 10)/1000 = 0.39$ $A_6 = 10$ $M_{ar} = 15.9$ (Same value as M_{ay}) $\alpha_2 = 0.39/15.9 = 0.025$
Yawing	Rolling					
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3-3 Load Factor of Dynamic Moment Find the dynamic moment M_e (N·m). Find the allowable dynamic moment M_{ea} (N·m). Find the load factor α_3 of the dynamic moment.	$M_e = 1/3 \cdot W_e \times 9.8 \times \frac{(L_n + A_n)}{1000}$ Collision equivalent to impact $W_e = \delta \cdot W \cdot V$ δ: Bumper coefficient With urethane bumper (Standard) = 4/100 With shock absorber = 1/100 Correction value of moment center position distance A_n: Table (3) $M_{ea} = K \cdot \gamma \cdot M_{max}$ Workpiece mounting coefficient K: Fig. (3) Allowable moment coefficient γ: Graph (2) Max. allowable moment M_{max}: Table (4) $\alpha_3 = M_e/M_{ea}$	<table><tr><th>Pitching</th><th>Yawing</th></tr><tr><td>Examine M_{ep}. $M_{ep} = 1/3 \times 16.8 \times 9.8 \times \frac{(30 + 10)}{1000} = 2.2$ $W_e = 4/100 \times 1 \times 420 = 16.8$ $A_2 = 10$ $M_{eap} = 1 \times 0.7 \times 15.9 = 11.1$ $K = 1$ $\gamma = 0.7$ $M_{pmax} = 15.9$ $\alpha_3 = 2.2/11.1 = 0.20$</td><td>Examine M_{ey}. $M_{ey} = 1/3 \times 16.8 \times 9.8 \times \frac{(30 + 31)}{1000} = 3.3$ $W_e = 16.8$ $A_4 = 31$ $M_{eay} = 11.1$ (Same value as M_{eap}) $\alpha_3 = 3.3/11.1 = 0.30$</td></tr></table>	Pitching	Yawing	Examine M_{ep} . $M_{ep} = 1/3 \times 16.8 \times 9.8 \times \frac{(30 + 10)}{1000} = 2.2$ $W_e = 4/100 \times 1 \times 420 = 16.8$ $A_2 = 10$ $M_{eap} = 1 \times 0.7 \times 15.9 = 11.1$ $K = 1$ $\gamma = 0.7$ $M_{pmax} = 15.9$ $\alpha_3 = 2.2/11.1 = 0.20$	Examine M_{ey} . $M_{ey} = 1/3 \times 16.8 \times 9.8 \times \frac{(30 + 31)}{1000} = 3.3$ $W_e = 16.8$ $A_4 = 31$ $M_{eay} = 11.1$ (Same value as M_{eap}) $\alpha_3 = 3.3/11.1 = 0.30$
Pitching	Yawing					
Examine M_{ep} . $M_{ep} = 1/3 \times 16.8 \times 9.8 \times \frac{(30 + 10)}{1000} = 2.2$ $W_e = 4/100 \times 1 \times 420 = 16.8$ $A_2 = 10$ $M_{eap} = 1 \times 0.7 \times 15.9 = 11.1$ $K = 1$ $\gamma = 0.7$ $M_{pmax} = 15.9$ $\alpha_3 = 2.2/11.1 = 0.20$	Examine M_{ey} . $M_{ey} = 1/3 \times 16.8 \times 9.8 \times \frac{(30 + 31)}{1000} = 3.3$ $W_e = 16.8$ $A_4 = 31$ $M_{eay} = 11.1$ (Same value as M_{eap}) $\alpha_3 = 3.3/11.1 = 0.30$					
3-4 Sum of Load Factors Possible to use if the sum of the load factors does not exceed 1.	$\sum \alpha_n = \alpha_1 + \alpha_2 + \alpha_3 \leq 1$	$\sum \alpha_n = \alpha_1 + \alpha_2 + \alpha_2' + \alpha_3 + \alpha_3' = 0.25 + 0.025 + 0.025 + 0.20 + 0.30 = 0.80 \leq 1$ And it is possible to use.				

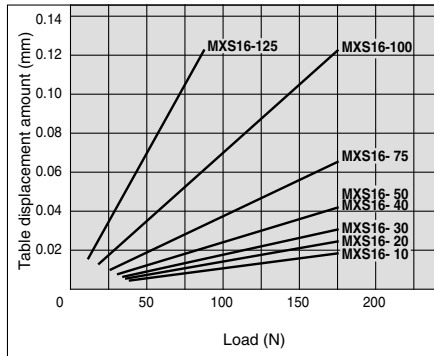
The graphs below show the table displacement when the static moment load is applied to the table. The graphs do not show the loadable mass. Refer to the Model Selection for the loadable mass.

Table displacement due to pitch moment load

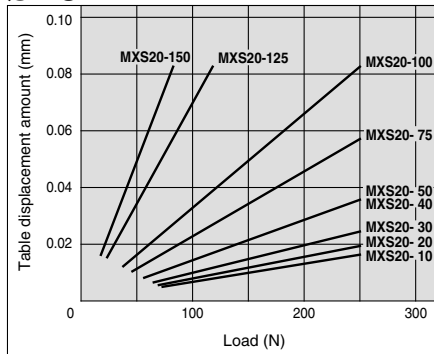
Table displacement when loads are applied to the section marked with the arrow at the full stroke.



ø16



ø20



ø25

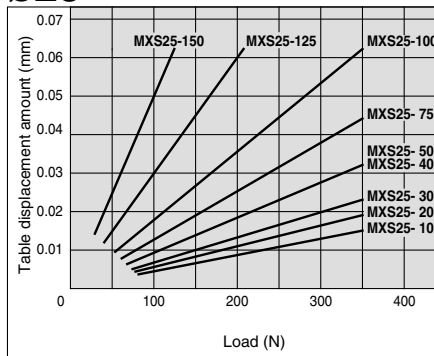
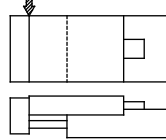
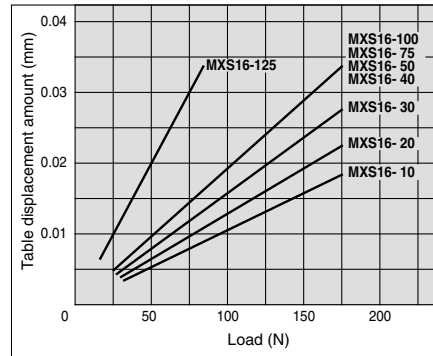


Table displacement due to yaw moment load

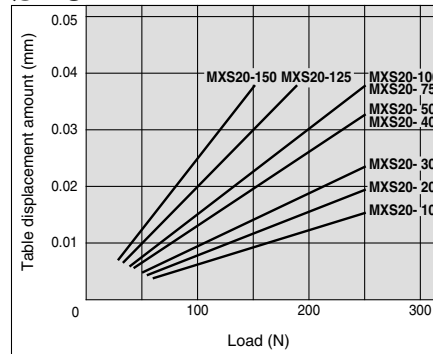
Table displacement when loads are applied to the section marked with the arrow at the full stroke.



ø16



ø20



ø25

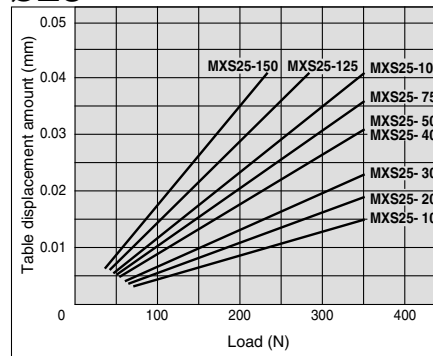
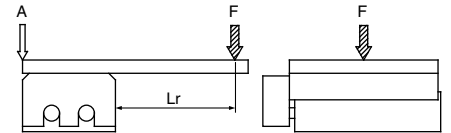
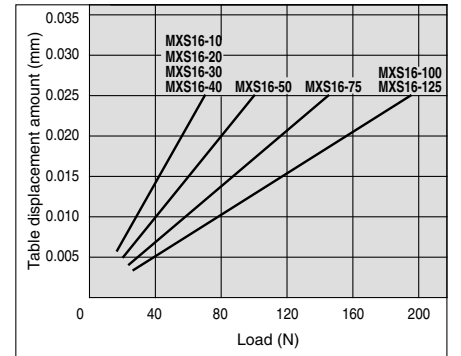


Table displacement due to roll moment load

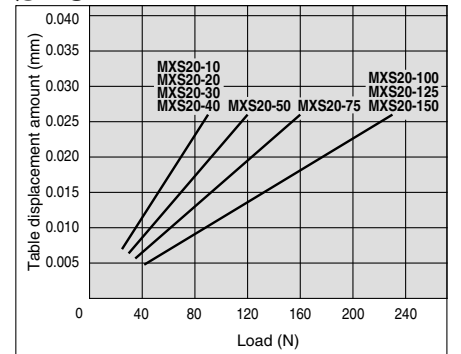
Table displacement of section A when loads are applied to the section F with the slide table retracted.



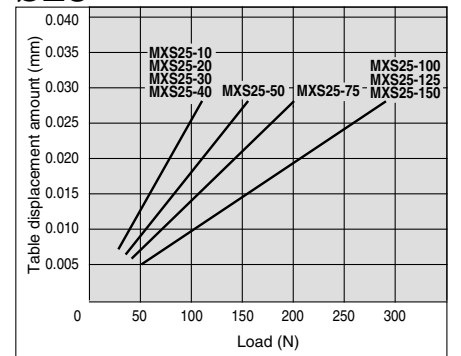
ø16



ø20



ø25



MXH

MXU

MXS

MXQ

MXF

MXW

MXJ

MXP

MXV

MTS

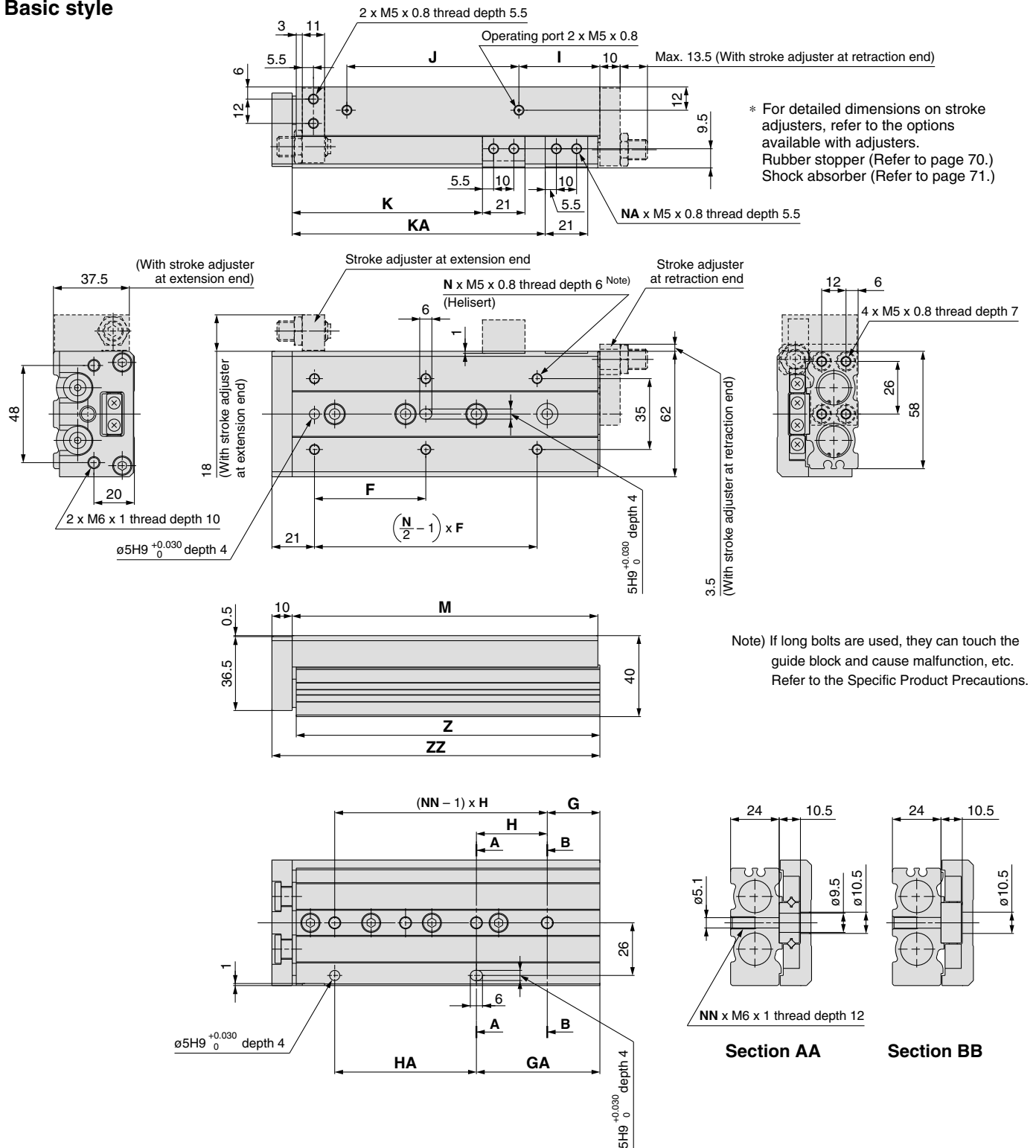
D-□

-X□

Individual
-X□

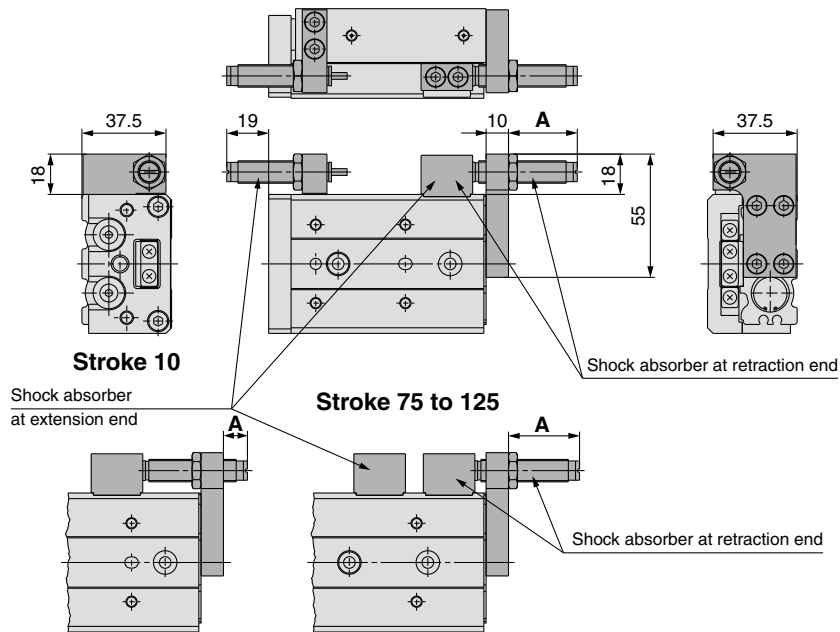
Dimensions: MXS16

Basic style



Model	F	N	G	H	NN	GA	HA	I	J	K	KA	NA	M	Z	ZZ
MXS16-10	35	4	16	40	2	16	40	10	40	29	—	2	76	75	87
MXS16-20	35	4	16	40	2	16	40	10	40	39	—	2	76	75	87
MXS16-30	35	4	16	40	2	16	40	10	40	49	—	2	76	75	87
MXS16-40	40	4	16	50	2	16	50	10	50	59	—	2	86	85	97
MXS16-50	30	6	21	30	3	51	30	15	60	69	—	2	101	100	112
MXS16-75	55	6	26	35	4	61	70	40	85	94	125	4	151	150	162
MXS16-100	65	6	39	35	5	109	70	55	118	119	173	4	199	198	210
MXS16-125	70	8	19	35	7	159	70	68	155	144	223	4	249	248	260

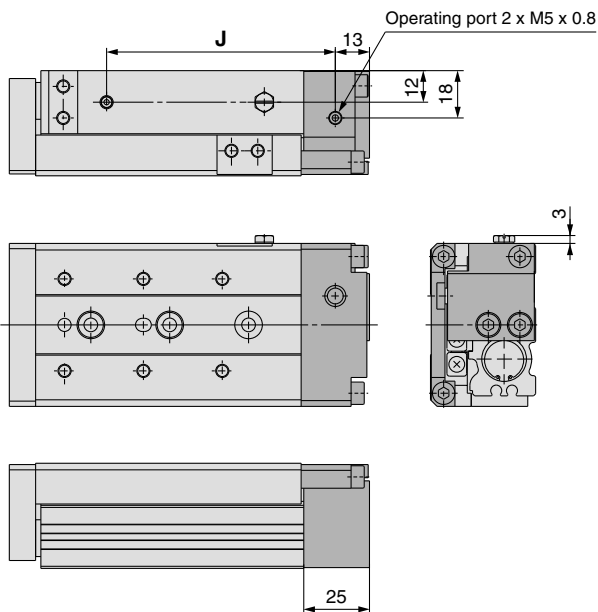
With shock absorber (ø16) MXS16-□□BS/BT/B



* Other dimensions are the same as the basic style.

Model	Stroke adjustment range		A dimension (Retracted side mounting)
	Extension end	Retraction end	
MXS16-10	Maximum 25	5	11
MXS16-20		10	21
MXS16-30		20	31
MXS16-40		20	31
MXS16-50		15	26
MXS16-75		20	32
MXS16-100		20	32
MXS16-125		20	32

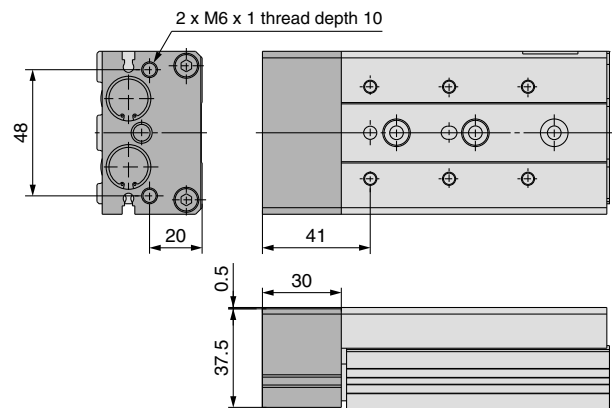
With end lock (ø16) MXS16-□□R



Model	J (mm)
MXS16-10R	62
MXS16-20R	62
MXS16-30R	62
MXS16-40R	72
MXS16-50R	87
MXS16-75R	137
MXS16-100R	185
MXS16-125R	235

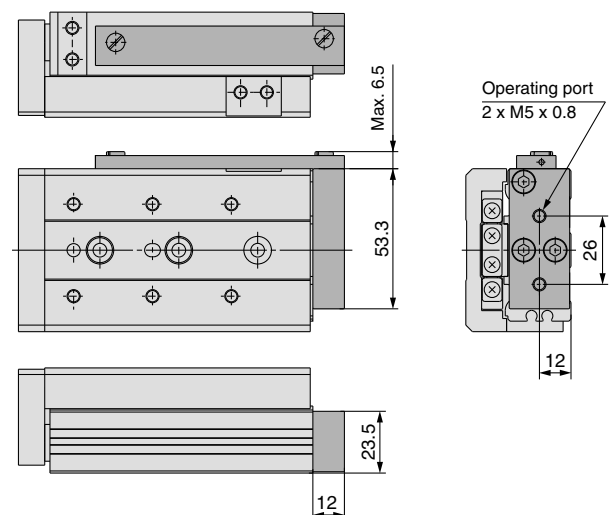
* Other dimensions are the same as the basic style.

With buffer (ø16) MXS16-□□F



* Other dimensions are the same as the basic style.

Axial piping type (ø16) MXS16-□□P



* Other dimensions are the same as the basic style.

MXH

MXU

MXS

MXQ

MXF

MXW

MXJ

MXP

MXV

MTS

D-□

-X□

Individual
-X□